

# Reconstruction of the radial refractive index profile of optical waveguides from lateral diffraction patterns

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- 2 Theory
  - Mie theory for cylinders
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- 6 Conclusion and outlook

## Motivation

- **Fibres** in communication technology (waveguides)
- Distinct types: Gradient and step-index fibres
- Desired: Measurement and control of parameters (refractive index profile) during production, i.e. the drawing process

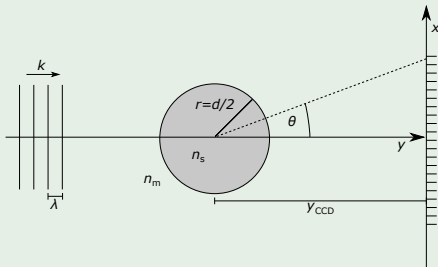
## Current knowledge

- Methods exist for the determination of the outer diameter
- These methods work well for **intransparent** cylinders
- No algorithm is known for the refractive index profile  $n(d)$  or  $\{d_j, n_j\}$

## General approach

- Illumination of a cylinder with plane-wave incidence,  $\zeta = 90^\circ$
- Refraction on layer boundaries and diffraction on edges
- Diffraction pattern is measured through an array of CCD cells
- Evaluation of the diffraction pattern for parameter determination

## Experimental setup



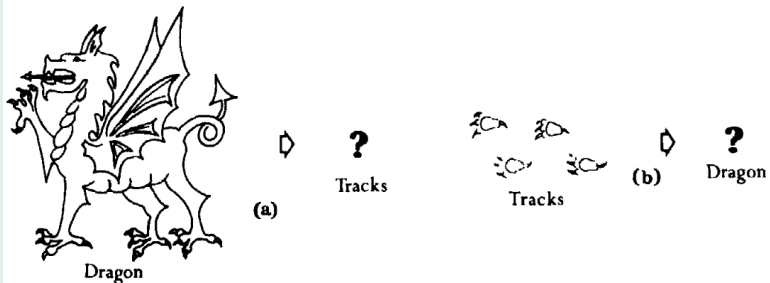
## Please note

- Setup is the same for stratified cylinders
- Distance  $y_{\text{CCD}}$  has to be known accurately
- All effects add up to scattering

## Theoretical approach: Inverse problem

- Direct problem: Parameters known, result unknown
- Inverse problem: Result known, parameters unknown

## Illustration of an inverse problem in [Bohren & Huffman 1983]



**Figure 1.5** (a) The direct problem: Describe the tracks of a given dragon. (b) The inverse problem: Describe a dragon from its tracks.

## Light scattering: Basics of Mie theory

- Propagation of EM waves is expressed through Maxwell equations
- Especially: Vector wave equation  $\nabla^2 \vec{E} + k^2 \vec{E} = 0$  and continuity at boundaries,  $[\vec{E}_2 - \vec{E}_1] \times \hat{n} = 0$
- Mie theory: Transformation to specific coordinates corresponding to geometry allows **expansion of scattered fields into Bessel functions**

## Scattering on cylinders

- Incident wave:  $\vec{E}_i = \sum_{n=-\infty}^{\infty} E_n \vec{N}_n^{(1)}$
- Scattered wave:  $\vec{E}_s = \sum_{n=-\infty}^{\infty} E_n [b_{nI} \vec{M}_n^{(3)} + ia_{nI} \vec{N}_n^{(3)}]$
- For normal incidence ( $\zeta = 90^\circ$ ), only  $z$ -components of  $\parallel$ -polarized

components are relevant:

$$E_{s\parallel}(z) = - \sum_{n=-\infty}^{\infty} E_n b_{n\parallel} N_n(z)$$



## Scattering coefficients

- General calculation for homogeneous ( $r = 1$ ) or stratified ( $r > 1$ ) cylinders:

$$b_n = \frac{m_r J_n(x_r)[J'_n(m_r x_r) + T_n^{r-1} N'_n(m_r x_r)] - J'_n(x_r)[J_n(m_r x_r) + T_n^{r-1} N_n(m_r x_r)]}{m_r H_n(x_r)[J'_n(m_r x_r) + T_n^{r-1} N'_n(m_r x_r)] - H'_n(x_r)[J_n(m_r x_r) + T_n^{r-1} N_n(m_r x_r)]} \quad (1)$$

$$T_n^s = \frac{m_s J_n(x_s)[J'_n(m_s x_s) + T_n^{s-1} N'_n(m_s x_s)] - J'_n(x_s)[J_n(m_s x_s) + T_n^{s-1} J_n(m_s x_s)]}{m_s J_n(x_s)[J'_n(m_s x_s) + T_n^{s-1} N'_n(m_s x_s)] - N'_n(x_s)[J_n(m_s x_s) + T_n^{s-1} J_n(m_s x_s)]} \quad (2)$$

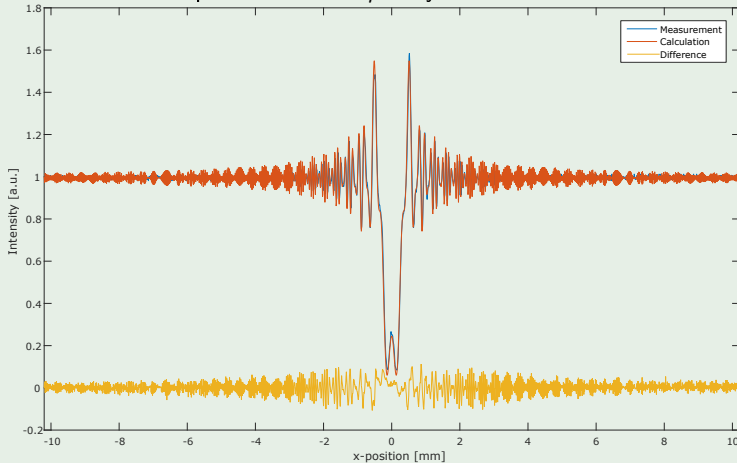
- Recursive calculation: Layers  $s = 1 \dots r$ , start with  $T_0 = \{0\}$
- Depends only on the relative refractive index  $m_s = \frac{n_s}{n_{s+1}}$  and the “size parameter”  $x_s = k_{s+1} \cdot r_s$  of the  $s$ -th layer

## Outline of the calculation of the diffraction pattern

- 1 Calculate scattering coefficients  $b_n$  up to  $n_{\max} = \lceil x + 4 \cdot \sqrt[3]{x} + 2 \rceil$
- 2 Transform CCD array to polar coordinates  $(x, y) \mapsto (\rho, \varphi)$
- 3 Calculate vector-harmonic generating functions  $N_n(z)$  for these coordinates
- 4 Calculate sum  $E_{s\parallel}(z) = - \sum_{-n_{\max}}^{n_{\max}} E_n b_{n\parallel} N_n(z)$ .

...and it works!

Agreement for an intransparent  $d = 370 \mu\text{m}$  cylinder,  $\lambda = 632.8 \text{ nm}$





## Inverse problem (now formally...)

- Generally, a **operator**  $\mathcal{F}$  on a **parameter set**  $r$  creates (maps to) a **far-field pattern**  $u_\infty$ , i.e. a simple operator equation:

$$\boxed{\mathcal{F} : r \mapsto u_\infty} \quad \text{or} \quad \boxed{\mathcal{F}(r) = u_\infty} \quad (3)$$

- **Direct** problem:  $\mathcal{F}$  and  $r$  are known,  $u_\infty$  is to be determined
- **Inverse** problem:  $\mathcal{F}$  and  $u_\infty$  are known,  $r$  is sought

## Solution of the inverse scattering problem

- Solution through the iteratively regularized Gauss-Newton (IRGN) algorithm:

$$\boxed{\|\mathcal{F}'[r_n]h_n + \mathcal{F}(r_n) - u_\infty^\delta\|^2 + \alpha_n\|h_n + r_n^\delta - r_0\|^2 \stackrel{!}{=} \min} \quad (4)$$

- In each iteration  $n$ : Calculate alteration  $h_n$  of the parameter set  $r_n$
- Iteration terminates after  $N$  steps, if  $\|\mathcal{F}(r_N) - u_\infty^\delta\|_2 \leq \tau\delta$

## Regularisation

- Special treatment for noisy data, weighting of far-field pattern
- The step update  $h_n$  of parameters  $r_n$  is calculated according to

$$h_n = - \frac{F'[r_n^\delta]^* (F(r_n^\delta) - u_\infty^\delta) + \alpha_n (r_n^\delta - r_0)}{F'[r_n^\delta]^* F'[r_n^\delta] + \alpha_n I} \quad (5)$$

with regularisation parameter  $\alpha_n = \alpha_0^n, \alpha_0 = 1/2$

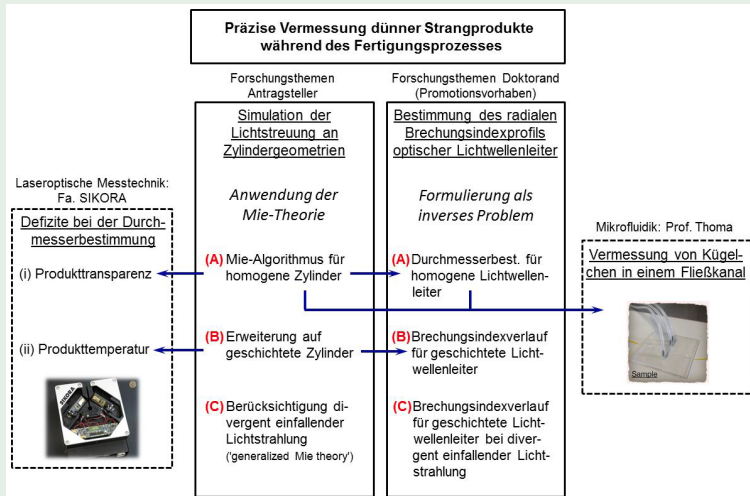
## Notes

- Derivative  $\mathcal{F}'[r_n]$  to the parameters  $r_n$  has to be known
- For homogeneous cylinders: Analytically...
- For stratified cylinders: Numerically...
- Analytical calculation does *not* pay off via a considerable time advantage!

## General properties

- Research project at Jade Hochschule
- Applied and carried out by Prof. Dr. Werner Blohm since 2014
- Aim: Improvement of the precision of diffraction-optics methods
- Doctoral research is embedded in the project through **Jade2Pro**
- Several related “milestones” have been proposed for both the applicant (Prof. Blohm) and the doctoral researcher (me)
- “Applicant” side ended in 2016, but research will be supported further

## Structogram of the Project



## Formal development of the doctorate

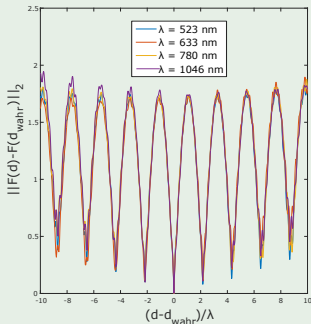
- Cooperation with Zentrum für Technomathematik (ZeTeM), Fachbereich 3, Bremen University
- Supervision by Prof. Dr. Armin Lechleiter, head of AG Inverse Probleme
- Guest in Bremen in WS 2015/16, seminar talk
- Beginning of WS 2016/17: Ph.D. student at Bremen
- In WS 2016/17: **Recognition of the research topic** by FB3
- Complete Title: “*Bestimmung des radialen Brechungsindexprofils optischer Lichtwellenleiter aus lateralen Streulichtverteilungen*”
- In WS 2016/17: Project **successfully evaluated** by Jade2Pro

## Project-related “publicity” so far

- Talks at 2nd, 3rd und 5th Jade2Pro-Kolloquium, Oldenburg
- Poster presentation at the DPG Spring Meeting 2017 of the Atomic, Molecular, Plasma Physics and Quantum Optics Section (SAMOP), Mainz

## The actual inverse scattering problem

- Operator  $\mathcal{F}$ : Mie theory for cylinder scattering
- Parameters  $r$ : Only diameter  $d$ , everything else is fixed ( $n_s, n_m, y_{\text{CCD}}, \lambda$ )
- Far-field  $u_\infty$ : Pattern on CCD array at distance  $y_{\text{CCD}}$
- Fréchet derivative  $\mathcal{F}'$  for  $d$  is analytically known



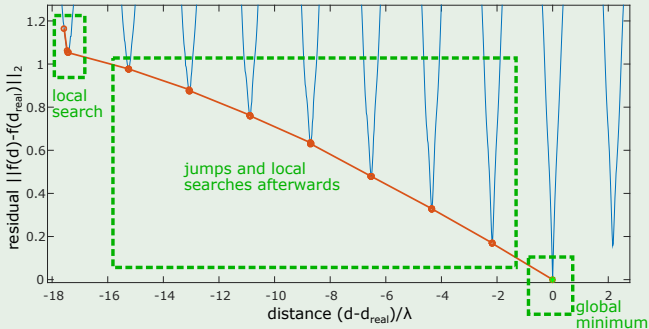
## Encountered “problem”

- Over  $d$ , the patterns resemble each other
- An IRGN algorithm iteratively minimizes the residual  $\|\mathcal{F}(d) - u_\infty\|_2$
- The residual, when compared to a reference  $d_{\text{real}}$ , exhibits local minima...
- **Ill-posed problem** (i.e. non-bijective)
- **Danger of false convergence**

## “Solution”: Modification of the IRGN algorithm

- But: Minima are spaced **periodically** by  $\delta_{\min,s} \approx 2.18\lambda$
- This property may be utilized...  
⇒ Detect local convergence and then “jump” by  $\pm 2.18\lambda$

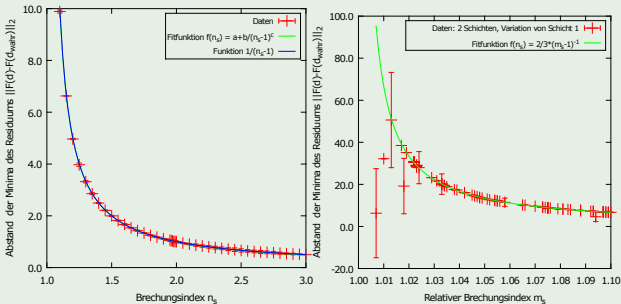
## Example for such a way of the algorithm



Where does the periodicity  $\delta_{\min,s} \approx 2.18$  stem from?

- In the present case,  $n_s = 1.458 \equiv m_s = \frac{n_s}{n_m} \dots$
- Research: Compare diffraction patterns for a range of  $d$  with a reference  $d_{\text{ref}}$  for several values of  $m_s$ , measure minima spacing...

## Dependence of minima spacing



## Result

$$\delta_{\min,s} = \frac{1}{m_s - 1}$$

...thus:

$$\frac{1}{1.458 - 1} = 2.183\dots$$

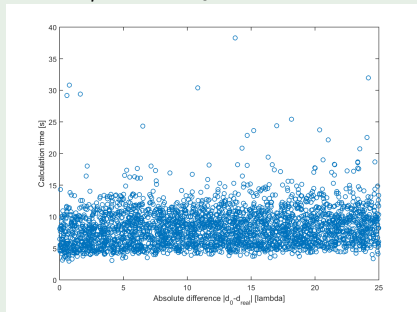
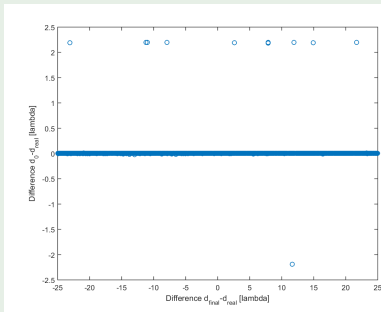


## Ideas for further improvement

- Improvement of initial values: Sample for a few values of  $d$  around  $d_0$ , choose value of least residual
- **Approximation through intransparent cylinders:**
  - Subtraction of the 3rd sinusoid component from the diffraction pattern approximates the pattern for a intransparent cylinder of the same  $d$
  - For intransparency, only a single global minimum exists...
  - GN iterations allow an approximation of  $d_0$  to  $d_{\text{real}}$
  - **Exact** determination of  $d_{\text{real}}$  is however not possible this way
- “**Plausibility check**”: Are minima also present at  $d_N$  for further observing angles  $\theta$ ? Otherwise, it's certainly no reliable result...

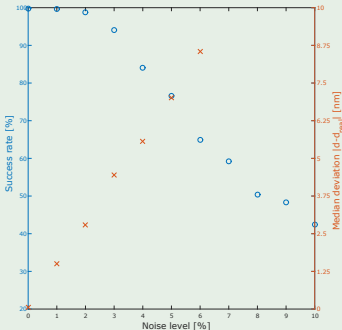
## Precision of the algorithm: Numerical evaluation

- $n = 1.4$ ,  $N = 2910$  random  $d_{\text{real}} = 110 \dots 150 \mu\text{m}$  and  $d_0 \in d_{\text{wahr}} \pm 25\lambda$



- The actual diameter  $d_{\text{real}}$  is met precisely (i.e.  $|d_N - d_{\text{real}}| < 0.1 \mu\text{m}$ , definition of a “success”) for 99.62% of the cases
- The calculation time exhibits no visible dependence on the distance between initial and actual values of  $d$

## Precision in presence of noise



- Noise: Multiplicative, normally distributed
- “Noise level”: Scaling factor for the width (variance) of the distribution
- Deviation of the result calculated only for “successful” cases
- Note: “Failures” still finish within local minima

## Summary

- Method for diameter determination is very precise
- Precision drops linearly with noise level
- Improvements lead to constant calculation times

## Basics

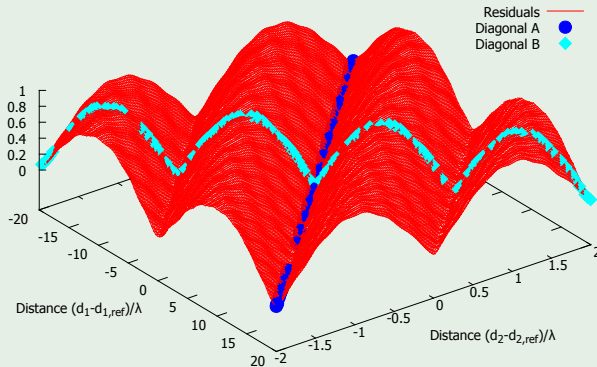
- **Aim:** Extension of the IRGN algorithm for stratified cylinders
- Calculation of diffraction patterns: Only different scattering coefficients
- Experience from homogeneous cylinders: Periodic local minima

## Expected difficulties

- Parameters to be found: Layer diameters  $d_j$
- More complex operation, more parameters must be optimised
- Especially: How can the “jumps” of the modified IRGN algorithm be implemented?

Example:  $J = 2$  layers,  $d_{\text{ref}} = [50, 120] \mu\text{m}$ ,  $n = [1.55, 1.5]$

Periodic behaviour and a global minimum at  $d \equiv d_{\text{ref}}$  exist

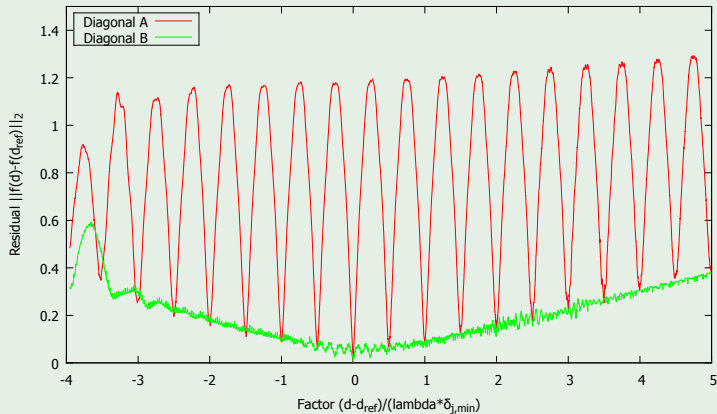


## Further findings

- Periodicity of minima for layer  $j < J$ : 
$$\delta_{\min,s} = \frac{2}{3} \frac{1}{m_s - 1}$$
- Remark: Refractive indices differ only marginally between layers,  $|n_j - n_{j+1}| = 0.001 \dots 0.02 \Rightarrow n_{j+1} = 1.5 : m_j \approx 1.000\bar{6} \dots 1.01\bar{3}$
- Thus: For inner layers “large” periodicity can be expected,  $\delta_{\min,s} \approx 50 \dots 1000\lambda$
- For the outermost layer  $j = J$  the jump from  $n_J$  to  $n_m$  is much larger  $\Rightarrow$  cf. homogeneous cylinder

## Even more further findings

The residuals along the diagonals in parameter space  $(d_1, d_2)$ :



## Ideas for layer diameter determination

- IRGN steps lead into a “trench”
- The “trench” is linear and described through the periodicities  $\delta_{j,\min}$
- Jumps should lead from one “trench” to another (diagonal A)
- Motion within one “trench”: local Minima (diagonal B)?
- **Summary:** A combination of IRGN, jumping and sampling methods seems promising for determining both diameters  $d_1$  and  $d_2$
- ...and how can that be applied to  $J > 2$ ?



## Aims to be reached

- **Milestone:** Algorithm for stratified cylinders is to be completed
- Experimental verification for homogeneous cylinder (experiment exists)
- Optionally: Generalized Lorenz-Mie theory for spherical waves

## Temporal constraints

- Current position is running until April 2018
- Probably extended by one year from remaining funds
- Current difficulty: A. Lechleiter out of office until further notice

## References

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Thanks for your attention!

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